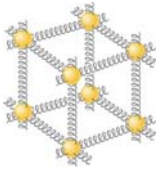


Introduction to Static/Dynamic Deformation with Mass-Spring Systems

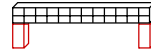


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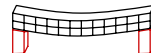
Static/Dynamic Deformation

- Static deformation
- Dynamic deformation



undeformed shape

$$f_{\text{internal}} \uparrow + f_{\text{external}} \downarrow = f_{\text{inertia}} =$$

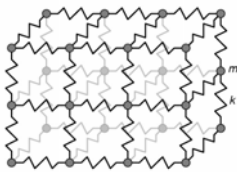


deformed shape



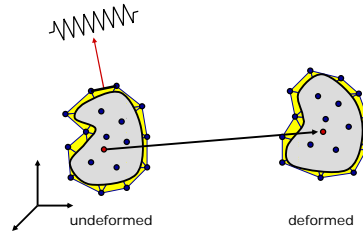
Mass-Spring Systems

- Using spring forces to connect mass points



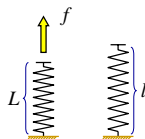
Mass-Spring Systems

- Using spring forces to connect mass points



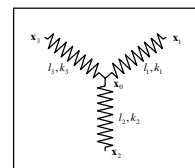
Elastic Springs

- Spring characteristics
 - Stiffness constant: k
 - Initial spring length: l
 - Current spring length: L
- Hooke's law: $f = k(L - l)$



Forces at the Mass Points

- Internal force f_i^{int}
 - $f_0^{\text{int}} = \sum_{i=1}^3 k_i (\|x_i - x_0\| - l_i) \frac{x_i - x_0}{\|x_i - x_0\|}$
- External force f_i^{ext}
 - Gravity, etc.
- Resulting force $f_i = f_i^{\text{int}} + f_i^{\text{ext}}$



model problem

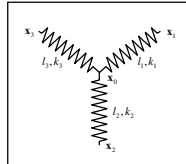
Static Equilibrium

- System of mass points

$$\mathbf{f}^{\text{int}} = \mathbf{K}(\mathbf{x})$$

- Static equilibrium

$$\mathbf{f} = \mathbf{K}(\mathbf{x}) + \mathbf{f}^{\text{ext}} = 0$$



model problem

From Static Eq. to Dynamic Eq.

- Static equilibrium

$$\mathbf{f} = \mathbf{K}(\mathbf{x}) + \mathbf{f}^{\text{ext}} = 0 \quad \Rightarrow \quad \mathbf{f}(t) = \mathbf{K}(\mathbf{x}(t)) + \mathbf{f}^{\text{ext}} = 0$$

- Equation of motion

$$\mathbf{M} \frac{d^2 \mathbf{x}(t)}{dt^2} = \mathbf{f}(t)$$

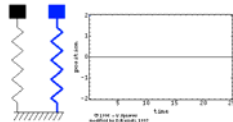
From Static Eq. to Dynamic Eq.

- Static equilibrium

$$\mathbf{f} = \mathbf{K}(\mathbf{x}) + \mathbf{f}^{\text{ext}} = 0 \quad \Rightarrow \quad \mathbf{f}(t) = \mathbf{K}(\mathbf{x}(t)) + \mathbf{f}^{\text{ext}} = 0$$

- Equation of motion with damping

$$\mathbf{M} \frac{d^2 \mathbf{x}(t)}{dt^2} + \mathbf{C} \frac{d\mathbf{x}(t)}{dt} = \mathbf{f}(t)$$



Mass-Spring Dynamics

- Equation of motion for mass point i at time t

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d\mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

acceleration
damping
spring + external

- 2nd order differential equation
- f is used for acceleration and damping
- Without damping term, simply $f = ma$

Numerical Integration

- 2nd order ODE \Rightarrow two coupled 1st order ODEs

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d\mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$



$$\begin{cases} \frac{d\mathbf{x}_i(t)}{dt} = \mathbf{v}_i(t) & \text{velocity} \\ \frac{d\mathbf{v}_i(t)}{dt} = \frac{\mathbf{f}_i(t) - c_i \mathbf{v}_i(t)}{m_i} & \text{acceleration} \end{cases}$$

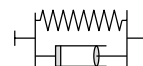
Damping Revisited

- Point damping

$$\frac{d\mathbf{v}_i(t)}{dt} = \frac{\mathbf{f}_i(t) - c_i \mathbf{v}_i(t)}{m_i}$$

- Damping force in opposite direction to the velocity

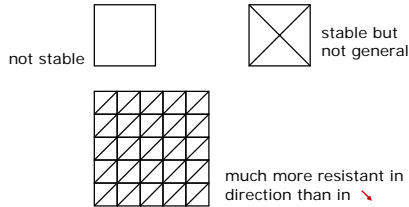
- Damped spring



- Damping force proportional to the velocity of the spring

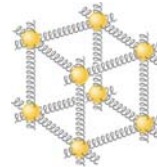
Topology and Stability

- Stability with respect to deformation



Requires well-chosen stable topologies!

Finite Element Method with Lumped Mass Formulation



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Mass-Spring Systems vs. FEM

- Mass-spring dynamics

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d \mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

- Explicit integration

$$\Delta \mathbf{x}_i = h(\dot{\mathbf{x}}_i + \Delta \dot{\mathbf{x}}_i)$$

$$\Delta \dot{\mathbf{x}}_i = \frac{h}{m_i} (\mathbf{f}_i - c_i \dot{\mathbf{x}}_i)$$

stable topology
appropriate constants

- Elasto-dynamic equations

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{f}$$

- Explicit integration

$$\Delta \mathbf{u} = h(\dot{\mathbf{u}} + \Delta \dot{\mathbf{u}})$$

$$\mathbf{M}\Delta \dot{\mathbf{u}} = h(\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$

matrix inversion
small displacements

Mass-Tensor Systems

- Mass-spring dynamics

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d \mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

- Explicit integration

$$\Delta \mathbf{x}_i = h(\dot{\mathbf{x}}_i + \Delta \dot{\mathbf{x}}_i)$$

$$\Delta \dot{\mathbf{x}}_i = \frac{h}{m_i} (\mathbf{f}_i - c_i \dot{\mathbf{x}}_i)$$

- Elasto-dynamic equations

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{f}$$

- Explicit integration

$$\Delta \mathbf{u} = h(\dot{\mathbf{u}} + \Delta \dot{\mathbf{u}})$$

$$\mathbf{M}\Delta \dot{\mathbf{u}} = h(\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$

Providing force from strain energy rather than spring energy!

Lumped Mass Formulation

- Mass-spring dynamics

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d \mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

- Explicit integration

$$\Delta \mathbf{x}_i = h(\dot{\mathbf{x}}_i + \Delta \dot{\mathbf{x}}_i)$$

$$\Delta \dot{\mathbf{x}}_i = \frac{h}{m_i} (\mathbf{f}_i - c_i \dot{\mathbf{x}}_i)$$

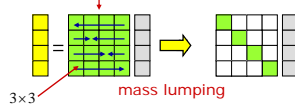
- Elasto-dynamic equations

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{f}$$

- Explicit integration

$$\Delta \mathbf{u} = h(\dot{\mathbf{u}} + \Delta \dot{\mathbf{u}})$$

$$\mathbf{M}\Delta \dot{\mathbf{u}} = h(\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$



Lumped Mass Formulation

- Mass-spring dynamics

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d \mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

- Explicit integration

$$\Delta \mathbf{x}_i = h(\dot{\mathbf{x}}_i + \Delta \dot{\mathbf{x}}_i)$$

$$\Delta \dot{\mathbf{x}}_i = \frac{h}{m_i} (\mathbf{f}_i - c_i \dot{\mathbf{x}}_i)$$

Mass Lumping

$$\Delta \mathbf{u} = h(\dot{\mathbf{u}} + \Delta \dot{\mathbf{u}})$$

$$\Delta \dot{\mathbf{u}} = h \mathbf{D}_m^{-1} (\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$

- Elasto-dynamic equations

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{f}$$

- Explicit integration

$$\Delta \mathbf{u} = h(\dot{\mathbf{u}} + \Delta \dot{\mathbf{u}})$$

$$\mathbf{M}\Delta \dot{\mathbf{u}} = h(\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$

$$\mathbf{D}_m \Delta \dot{\mathbf{u}} = h(\mathbf{f} - \mathbf{C}\dot{\mathbf{u}} - \mathbf{K}\mathbf{u})$$

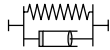
Mass-Spring vs. Lumped Mass FEM

Mass-spring dynamics

$$m_i \frac{d^2 \mathbf{x}_i(t)}{dt^2} + c_i \frac{d \mathbf{x}_i(t)}{dt} = \mathbf{f}_i(t)$$

Large displacements are supported inherently.

Damped spring



Adopt nonlinear visco-elastic formulation!

Elasto-dynamic equations

$$\mathbf{M} \ddot{\mathbf{u}} + \mathbf{C} \dot{\mathbf{u}} + \mathbf{K} \mathbf{u} = \mathbf{f}$$

Large displacements

$$\varepsilon_{ij} = \frac{\partial \mathbf{x}}{\partial u_i} \cdot \frac{\partial \mathbf{x}}{\partial u_j} - \delta_{ij}$$

Strain rate tensor

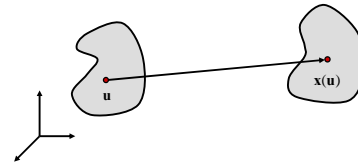
$$v_{ij} = \frac{\partial \dot{\mathbf{x}}}{\partial u_i} \cdot \frac{\partial \dot{\mathbf{x}}}{\partial u_j} + \frac{\partial \dot{\mathbf{x}}}{\partial u_i} \cdot \frac{\partial \dot{\mathbf{x}}}{\partial u_j}$$

Visco-Elastic Formulation

Green's strain tensor

$$\varepsilon_{ij} = \frac{\partial \mathbf{x}}{\partial u_i} \cdot \frac{\partial \mathbf{x}}{\partial u_j} - \delta_{ij} \quad \Rightarrow \quad \boldsymbol{\varepsilon} = \mathbf{J}^T \mathbf{J} - \mathbf{I}$$

$$\mathbf{J} = \left[\frac{\partial x_i}{\partial u_j} \right]_{b,3}$$



Visco-Elastic Formulation

Green's strain tensor

$$\varepsilon_{ij} = \frac{\partial \mathbf{x}}{\partial u_i} \cdot \frac{\partial \mathbf{x}}{\partial u_j} - \delta_{ij} \quad \Rightarrow \quad \boldsymbol{\varepsilon} = \mathbf{J}^T \mathbf{J} - \mathbf{I}$$

$$\mathbf{J} = \left[\frac{\partial x_i}{\partial u_j} \right]_{b,3}$$

Strain rate tensor

$$v_{ij} = \frac{d \varepsilon_{ij}}{dt} = \frac{\partial \dot{\mathbf{x}}}{\partial u_i} \cdot \frac{\partial \dot{\mathbf{x}}}{\partial u_j} + \frac{\partial \dot{\mathbf{x}}}{\partial u_i} \cdot \frac{\partial \dot{\mathbf{x}}}{\partial u_j} \quad \Rightarrow \quad \mathbf{v} = \mathbf{J}^T \dot{\mathbf{J}} + \dot{\mathbf{J}}^T \mathbf{J}$$

$$\mathbf{j} = \left[\frac{\partial \dot{x}_i}{\partial u_j} \right]_{b,3}$$

Visco-Elastic Formulation

Stress tensor

$$\boldsymbol{\sigma}^e = \lambda \operatorname{tr}(\boldsymbol{\varepsilon}) \mathbf{I} + 2\mu \boldsymbol{\varepsilon} \quad \boldsymbol{\sigma}^v = \phi \operatorname{tr}(\mathbf{v}) \mathbf{I} + 2\eta \mathbf{v}$$

elastic stress tensor viscous stress tensor

Strain energy

$$U^e = \frac{1}{2} \int_{\Omega} \sigma_{ij}^e \varepsilon_{ij} d\Omega \quad U^v = \frac{1}{2} \int_{\Omega} \sigma_{ij}^v v_{ij} d\Omega$$

elastic potential energy damping potential energy

Finite Element Discretization

Refer to the paper

James F. O'Brien and Jessica K. Hodgins
 Graphical Modeling and Animation of Brittle Fracture
 Computer Graphics (Proc. SIGGRAPH '99), pp. 137-146